

UNCLASSIFIED

AD 4 5 0 2 0 5

DEFENSE DOCUMENTATION CENTER

FOR

SCIENTIFIC AND TECHNICAL INFORMATION

CAMERON STATION ALEXANDRIA, VIRGINIA



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

450205

CONTRACT TECHNICAL NOTE

A NUMERICAL INVESTIGATION OF THE VALIDITY OF THE BORN APPROXIMATION FOR DETERMINATION OF THE REFLECTION COEFFICIENTS OF UNDERDENSE PLASMA SLABS

CONTRACT NO. DA-04-495-ORD-3567(Z)
HYPERVELOCITY RANGE RESEARCH PROGRAM
A PART OF PROJECT "DEFENDER"

GM DEFENSE RESEARCH LABORATORIES

SANTA BARBARA, CALIFORNIA



AEROSPACE OPERATIONS DEPARTMENT



CTN64-08

OCTOBER 1964

450205

TALOGED BY DDC

AS AD No.

NOTICE

The information presented in this Technical Note is preliminary and should not be interpreted as representing the final opinion of GM Defense Research Laboratories or the author on the subject. Further, to expedite prompt distribution of the technical contents, no attempt at an editorial review has been made.

CONTRACT TECHNICAL NOTE

**A NUMERICAL INVESTIGATION OF THE VALIDITY
OF THE BORN APPROXIMATION FOR
DETERMINATION OF THE REFLECTION COEFFICIENTS
OF UNDERDENSE PLASMA SLABS**

S. ZIVANOVIC

**THIS RESEARCH WAS SUPPORTED BY THE
ADVANCED RESEARCH PROJECTS AGENCY**

**DEPARTMENT OF DEFENSE
AND WAS MONITORED BY THE
U.S. ARMY MISSILE COMMAND
REDSTONE ARSENAL, ALABAMA**

GM DEFENSE RESEARCH LABORATORIES

SANTA BARBARA, CALIFORNIA



AEROSPACE OPERATIONS DEPARTMENT

**CONTRACT NO. DA-04-495-ORD-3567(Z)
HYPERVELOCITY RANGE RESEARCH PROGRAM
A PART OF PROJECT "DEFENDER"**

DDC AVAILABILITY NOTICE

Qualified requesters may obtain
copies of this report from DDC

CTN64-08

OCTOBER 1964

ABSTRACT

The validity of the Born approximation for determination of the reflection coefficients of plasma slabs is numerically examined for two cases: the uniform underdense plasma slab and a plasma slab with a sinusoidal electron density perturbation superimposed on a constant electron density. The regions of validity of the Born approximation are discussed in each case.

CONTENTS

	Page
ABSTRACT	i
I. INTRODUCTION	1
II. THEORY	2
Reflection and Transmission of EM Waves from Nonuniform Underdense Plasma Slabs	2
III. DISCUSSION OF RESULTS	4
IV. CONCLUSIONS	10
REFERENCES	10

ILLUSTRATIONS

Figure No.	Title	
1	Geometry of the Plasma Slab	2
2	Percentage Error in Reflection Coefficient of Uniform Plasma Slab for Born Approximation as a Function of Normalized Plasma Frequency, Normalized Thickness of the Slab, and Normalized Collision Frequency $\Omega_c = 0$	6
3	Percentage Error in Reflection Coefficient of Uniform Plasma Slab for Born Approximation as a Function of Normalized Plasma Frequency, Normalized Thickness of the Slab, and Normalized Collision Frequency $\Omega_c = 0.1$	7
4	Percentage Error in Reflection Coefficient of Uniform Plasma Slab for Born Approximation as a Function of Normalized Plasma Frequency, Normalized Thickness of the Slab, and Normalized Collision Frequency $\Omega_c = 0.2$	8
5	Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.05$	11
6	Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.1$	12

ILLUSTRATIONS (Cont'd)

Figure No.	Title	Page
7	Reflection Coefficient of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.2$ Dashed Line - Exact Values of Reflection Coefficient Solid Line Born Approximation of the Reflection Coefficient	13
8	Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.4$	14
9	Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.6$	15
10	Reflection Coefficient of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 1.0$ and $a = 5.25$ Colored Curve: Exact Values of Reflection Coefficient Black Curve: Born Approximation of the Reflection Coefficient	16
11	Reflection Coefficient of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 1.0$ and $a = 5.5$ Colored Curve: Exact Values of Reflection Coefficient Black Curve: Born Approximation of the Reflection Coefficient	17

I. INTRODUCTION

In the study of the propagation of electromagnetic waves through ionized gases it is seldom possible to get analytic solutions which are easy to interpret without tedious computing. Direct numerical solutions give accurate results, but they also fail to give physical insight into the mechanism of propagation. However, sometimes it is desirable to have an analytic solution which is easy to follow even if some accuracy has to be sacrificed.

The Born approximation, applied to the problem of EM scattering from an underdense plasma, serves this purpose. To use the Born approximation one has to assume that the incident wave is not changed by the medium through which it passes, and to neglect multiple scattering. It has been used often and, for example, Booker and Gordon^{(1)*} have used it successfully to solve the problem of scattering from small random inhomogeneities in the troposphere. A good discussion of the Born approximation is given in Schiff⁽²⁾ and other textbooks on quantum mechanics and wave propagation.

In this note, the Born approximation is used to derive the transmission and reflection coefficients of uniform and nonuniform plasma slabs for normal incidence. It is shown that the Born approximation gives very good results for the reflection coefficient of uniform slabs (within 8% up to plasma frequencies of 0.2 of incident frequency and slab thicknesses up to five wavelengths of incident wave). The transmission coefficient, calculated from the Born approximation, has a magnitude greater than unity but its phase shift is approximately correct. The reflection coefficient for a plasma in which there are harmonic variations in electron density is also calculated and compared with the exact results.

* Raised numbers in parentheses indicate references listed at the end of this report.

In this latter case the errors in the Born approximation are due mostly to the scattering from the outside boundaries of the plasma. It should be mentioned that a strong resonance occurs in the case when the wavelength of the fluctuations is exactly equal to one-half of the free-space wavelength. This result can be useful in studying the reflection from the turbulent wakes of hypersonic projectiles – a subject which will be treated in a subsequent note.

II. THEORY

Reflection and Transmission of EM Waves from Nonuniform Underdense Plasma Slabs

Let a plasma be confined to a slab of thickness d , located such that the z -axis is perpendicular to the slab, as depicted in Figure 1. Let a plane transverse electromagnetic wave propagating in the direction of the positive z -axis with its electric field E_i in the x direction be incident on the plasma slab. The electric field is given by

$$E_i = \hat{x} E_0 \exp [j(\omega t - kz)] \quad (1)$$

where E_0 is the complex amplitude of the incident wave, ω is the angular frequency of the wave, t is the time, $k=2\pi\lambda^{-1}$ and λ is the wavelength of the wave in free space.

It will be assumed that the first Born approximation is valid, i. e. , that the variations of E_i can be neglected throughout the plasma and also that the multiple scattering can be neglected, hence the incident field is the total field

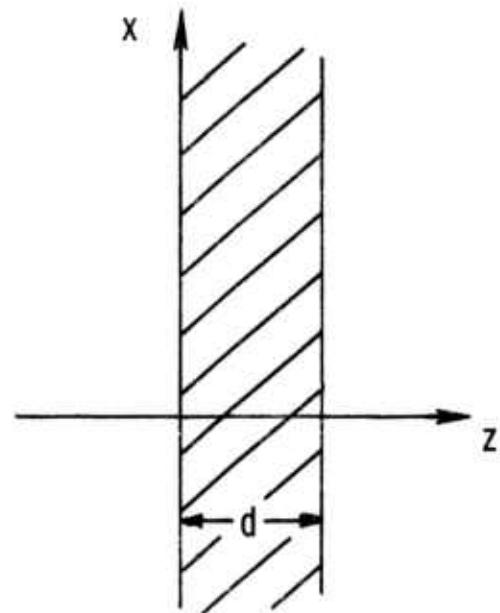


Figure 1 Geometry of the Plasma Slab

throughout the plasma. It will also be assumed that the properties of the plasma change only in the z-direction.

A uniform layer of plasma of thickness a will have the reflection coefficient⁽³⁾

$$R = \frac{E_r}{E_i} = \frac{(1 - \epsilon/\epsilon_0) \left[1 - \exp(-2jk \sqrt{\epsilon/\epsilon_0} a) \right]}{(\sqrt{\epsilon/\epsilon_0} + 1)^2 - (\sqrt{\epsilon/\epsilon_0} - 1)^2 \exp(-2jk \sqrt{\epsilon/\epsilon_0} a)} \quad (2)$$

where E_r and E_i are the complex amplitudes of the reflected and incident electromagnetic waves, respectively, evaluated at the incident side of the slab, and ϵ and ϵ_0 are the permittivity of the plasma and free space, respectively.

For an elementary slab of thickness $d\zeta$, located at ζ , expression (2) reduces to (subscript "e" stands for "elementary")

$$R_e = \frac{\epsilon - \epsilon_0}{2\epsilon_0} jk d\zeta = -\frac{jk}{2} \Delta d\zeta \quad (3)$$

where

$$\Delta \equiv \frac{\epsilon - \epsilon_0}{\epsilon_0} \quad (4)$$

or, if one defines the reflection coefficient as the ratio of the reflected-wave amplitude to the transmitted-wave amplitude at the origin,

$$R_e = -\frac{jk}{2} \Delta e^{-2jk\zeta} d\zeta \quad (5)$$

Within the validity of the Born approximation the reflection coefficient of the entire slab is

$$R = -\frac{jk}{2} \int_{\zeta=0}^a \Delta e^{-2jk\zeta} d\zeta \quad (6)$$

The transmission coefficient of a uniform plasma slab is

$$T = \frac{E_t}{E_i} = \frac{4\sqrt{\epsilon/\epsilon_0} \exp \left[-jk (\sqrt{\epsilon/\epsilon_0} - 1) a \right]}{(\sqrt{\epsilon/\epsilon_0} + 1)^2 - (\sqrt{\epsilon/\epsilon_0} - 1)^2 \exp \left[-2jk \sqrt{\epsilon/\epsilon_0} a \right]} \quad (7)$$

where E_t is the amplitude of the transmitted wave and E_t and E_i are evaluated at the same point. For infinitesimal thickness

$$T_e = 1 - jk d \left[(\sqrt{\epsilon/\epsilon_0} - 1) - \frac{1}{2} (\sqrt{\epsilon/\epsilon_0} - 1)^2 \right] \quad (8)$$

Retaining only the first power in $(\sqrt{\epsilon/\epsilon_0} - 1)$, (8) becomes

$$T_e = 1 - jk (\sqrt{\epsilon/\epsilon_0} - 1) d \quad (9)$$

The change in the transmitted wave due to the elementary plasma slab is represented by the second term in the right-hand side in (9). The total transmission coefficient is hence

$$T_e = 1 - jk \int_0^a (\sqrt{\epsilon/\epsilon_0} - 1) d\zeta \quad (10)$$

The phase shift in the transmitted wave is hence (for negligible losses, that is, pure real ϵ)

$$\angle T = -\arctan k \int_0^a (\sqrt{\epsilon/\epsilon_0} - 1) d\zeta \approx -\arctan \frac{k}{2} \int_0^a \Delta d\zeta \quad (11)$$

III. DISCUSSION OF RESULTS

The magnitude of the transmission coefficient for real ϵ in the Born approximation is always greater than one, and, hence, physically meaningless.

However, for small Δ (10) will give the phase shift with an accuracy which

will depend on the thickness of the medium and the magnitude of Δ . Also (10) gives an indication that, at least for small Δ , the angle of T depends only on the average properties of the medium.

The reflection coefficient (6) is a function of the changes of Δ throughout the plasma and, for small Δ , the errors made by using (6) instead of the exact reflection coefficient are small. To illustrate this point, on Figures 2 to 4, the error

$$\epsilon = \left| \frac{R - R_a}{R} \right| 100 \quad (12)$$

where R is the exact value of the reflection coefficient for the uniform plasma and R_a is computed from (6) assuming constant Δ , is plotted. In a slightly ionized plasma⁽⁴⁾

$$\Delta = -\frac{\Omega_p^2}{1 - j\Omega_c} \quad (13)$$

where $\Omega_p^2 \equiv (q^2 n) / (\epsilon_0 m \omega^2)$, q is the charge of an electron, m is its mass, n is the electron density, $\Omega_c \equiv \nu_c / \omega$ and ν_c is the collision frequency between electrons and neutral atoms. It is seen that the error does not exceed a few percent for $\Omega_p \leq 0.2$ and $\Omega_c \leq 0.2$.

If the electron density has a periodic component, i. e. , it can be expressed as

$$n = n_0 + n_1 \sin(k_1 z + \theta) \quad (14)$$

where $n_0 > n_1$ and n_1 and k_1 are constants, then, assuming constant collision frequency, Δ can be expressed as

$$\Delta = -\frac{\Omega_p^2}{1 - j\Omega_c} (1 + h \sin k_1 z) \quad (15)$$

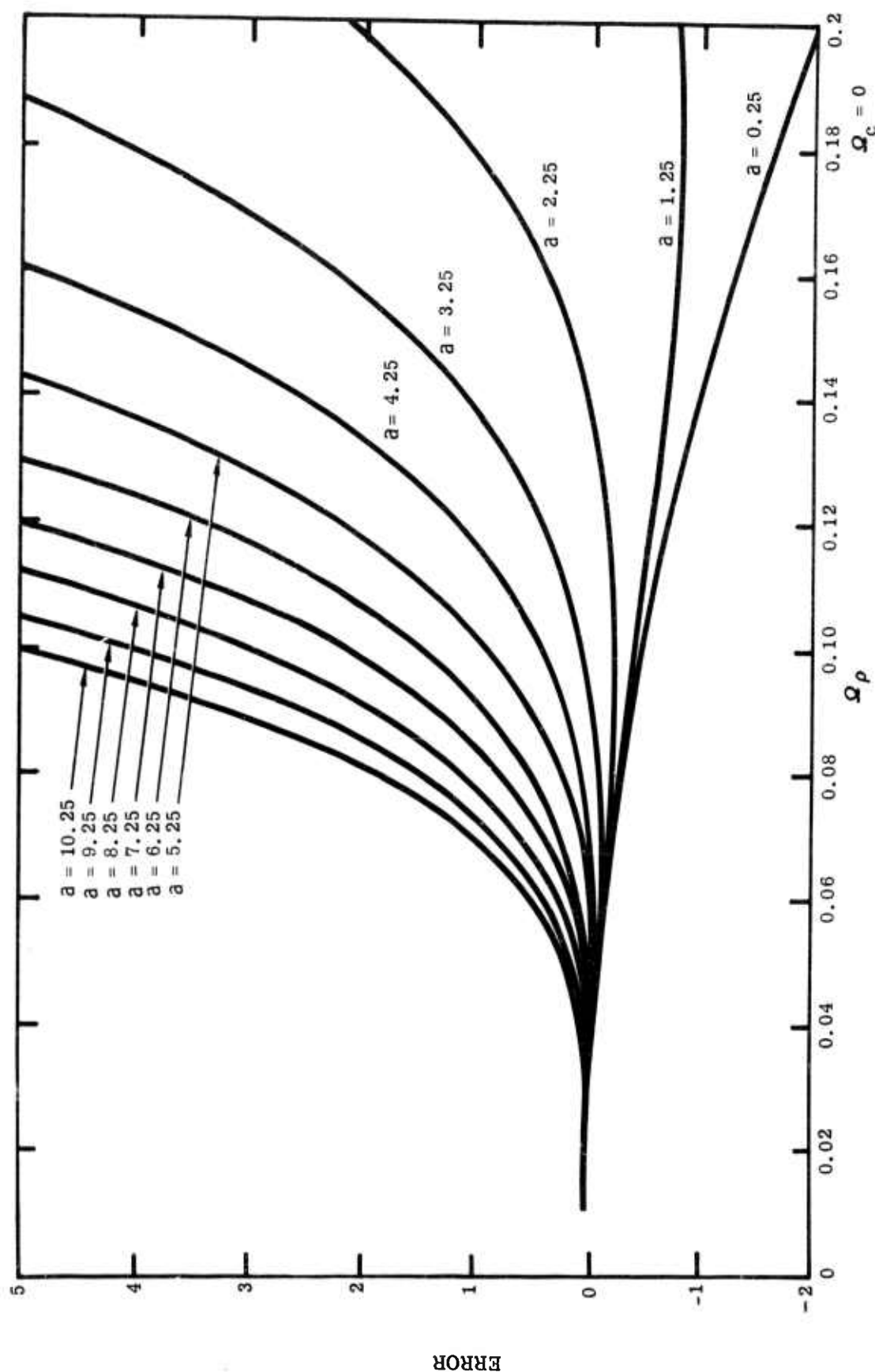


Figure 2 Percentage Error in Reflection Coefficient of Uniform Plasma Slab for Born Approximation as a Function of Normalized Plasma Frequency, Normalized Thickness of the Slab, and Normalized Collision Frequency $\Omega_c = 0$

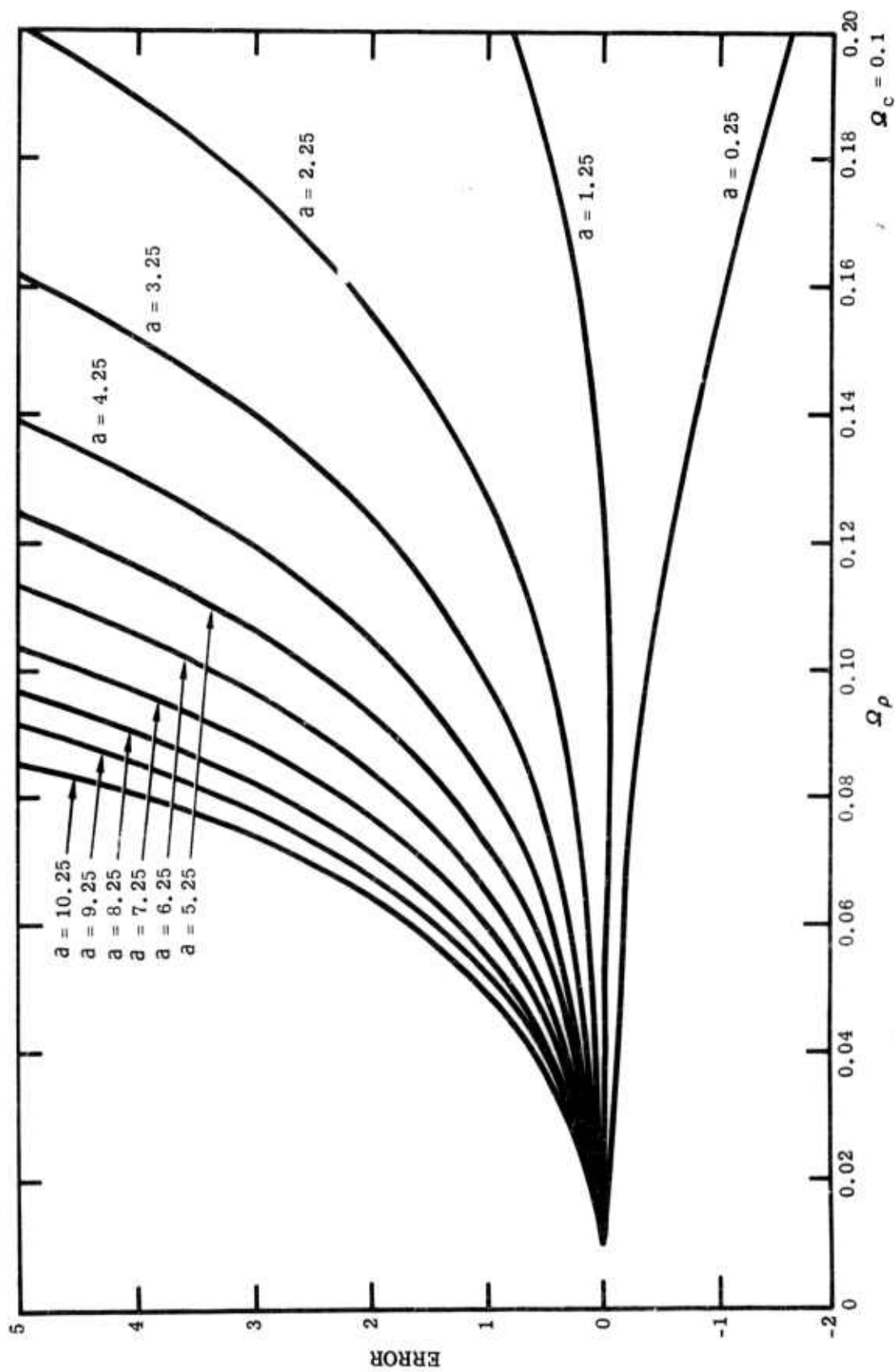


Figure 3 Percentage Error in Reflection Coefficient of Uniform Plasma Slab for Born Approximation as a Function of Normalized Plasma Frequency, Normalized Thickness of the Slab, and Normalized Collision Frequency $\Omega_c = 0.1$

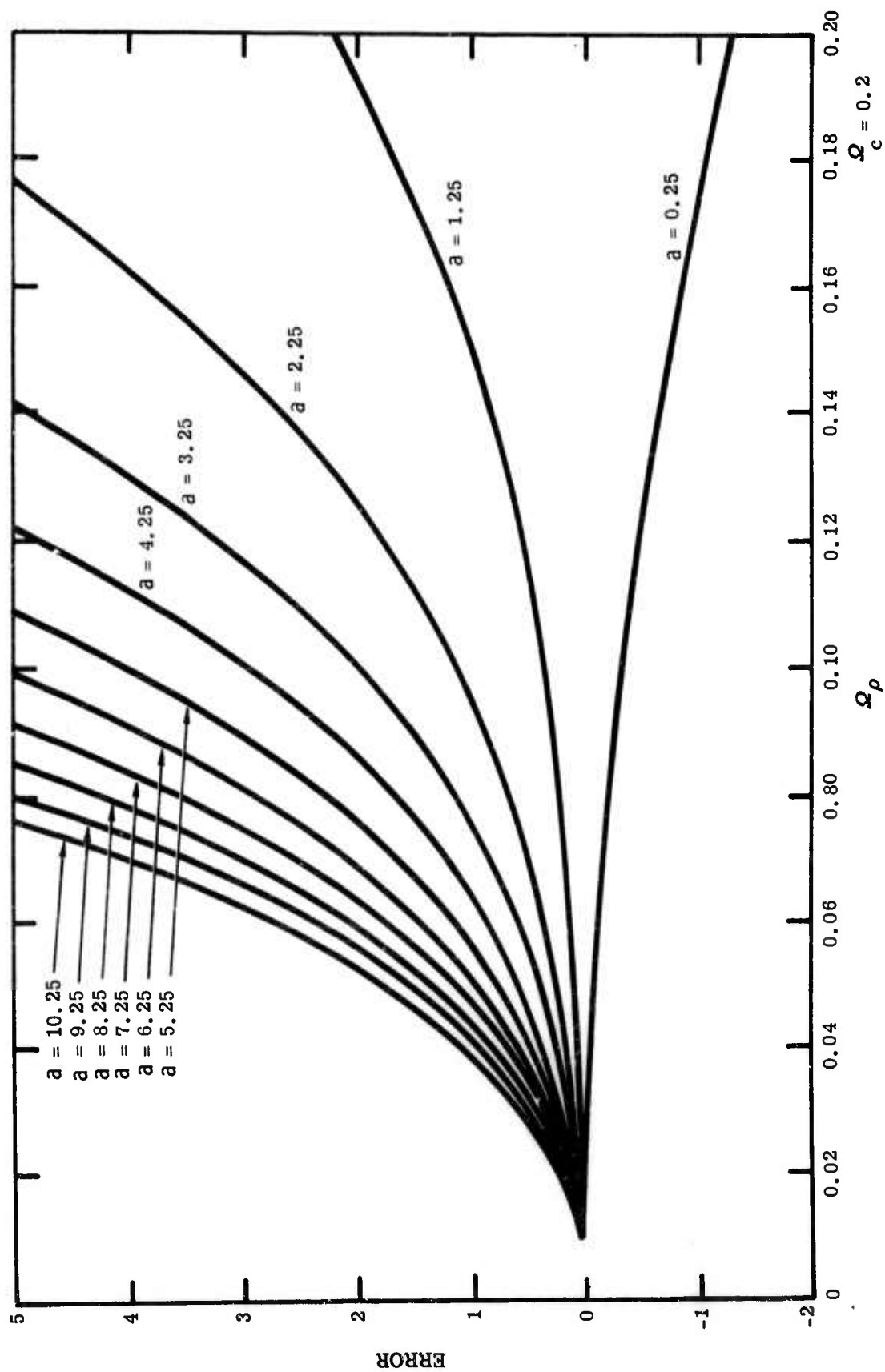


Figure 4 Percentage Error in Reflection Coefficient of Uniform Plasma Slab for Born Approximation as a Function of Normalized Plasma Frequency, Normalized Thickness of the slab, and Normalized Collision Frequency $\Omega_c = 0.2$

where $\Omega_{po}^2 = (q^2 n_o) (\epsilon_o m \omega^2)^{-1}$ and $h \equiv n_1/n$. Substituting expression (15) into (6) gives

$$R = \frac{k \Omega_{po}^2}{2j(1-j\Omega_c)} \int_0^a (1 + h \sin k_1 \zeta) e^{-2jk\zeta} d\zeta \quad (16)$$

Integrating, one has

$$R = \frac{\Omega_{po}^2}{4(1-j\Omega_c)} \left\{ \left[1 - e^{-j2ka} \right] + h(ka) \left[\frac{e^{ja(k_1-2k)} - 1}{ja(k_1-2k)} + \frac{e^{-ja(k_1+2k)} - 1}{ja(k_1+2k)} \right] \right\} \quad (17)$$

The first term on the right-hand side represents the Born approximation for the reflection from a uniform plasma, i.e., for $h=0$. The second term represents the contribution due to the periodicity of the plasma.

It is obvious that for $k_1=2k$ a strong resonance occurs. For $k_1=2k=4\pi/\lambda$ expression (18) becomes

$$R = \frac{\Omega_{po}^2}{4(1-j\Omega_c)} \left\{ \left[1 - e^{-2kja} \right] + 2\pi h \frac{a}{\lambda} \left[1 + j \frac{1 - e^{-4jka}}{4ka} \right] \right\} \quad (18)$$

and hence, a ripple in electron density equal to only 20% of the average electron density can enhance the reflection of the plasma ten wavelengths long by over six times (about 16 db in power).

Off resonance, the contribution of the harmonic part of the electron density decreases rapidly and fluctuates around the reflection coefficient for a uniform plasma.

To illustrate the accuracy of the Born approximation, in Figures 5 to 11 the square of the magnitude of the reflection coefficient for the plasma with electron density distribution given by (14) is plotted versus the density wavelength $M = 2\pi/k_1$, as calculated from expression (17). Then, for $h = 0.2$ and $h = 1$ the exact values of reflection coefficient obtained by using an exact numerical technique⁽⁵⁾ are given for comparison. It is seen that the agreement between the two curves is good and that the main difference comes from the uniform component of electron density (change of the effective thickness of plasma). Around the resonances ($M=1/2$) agreement is, for most practical purposes, very good. The vertical scale is expressed in decibels below the unity reflection coefficient because the square of the reflection coefficient as defined by (2) is the power reflection coefficient.

IV. CONCLUSIONS

It is seen that, depending on the required accuracy, the Born approximation can be a very satisfactory approach for studying the reflections from underdense plasmas – up to plasma frequencies of about 0.2 of incident frequency. Its chief merit lies in its simplicity and ability to handle nonuniform plasmas.

REFERENCES

1. Booker and Gordon, "A Theory of Radio Scattering in the Troposphere," Proceedings of the I. R. E. Vol. 38, No. 4, Apr 1950, pp. 401 – 412
2. L. Schiff, Quantum Mechanics, Second Edition, McGraw Hill, 1955
3. W. M. Cady, M. B. Karelitz and L. A. Turner, Radar Scanners and Radomes, Radiation Laboratory Series, McGraw Hill, 1948 p. 354
4. E. C. Jordan, Electromagnetic Waves and Radiating Systems, Prentice-Hall, Inc., 1950, p. 661
5. S. Zivanovic: "A Numerical Method for the Determination of the Transmission and Reflection Coefficients of a Non-Uniform Plasma Slab," GM Defense Research Laboratories Report TR62-209J, Dec 1962

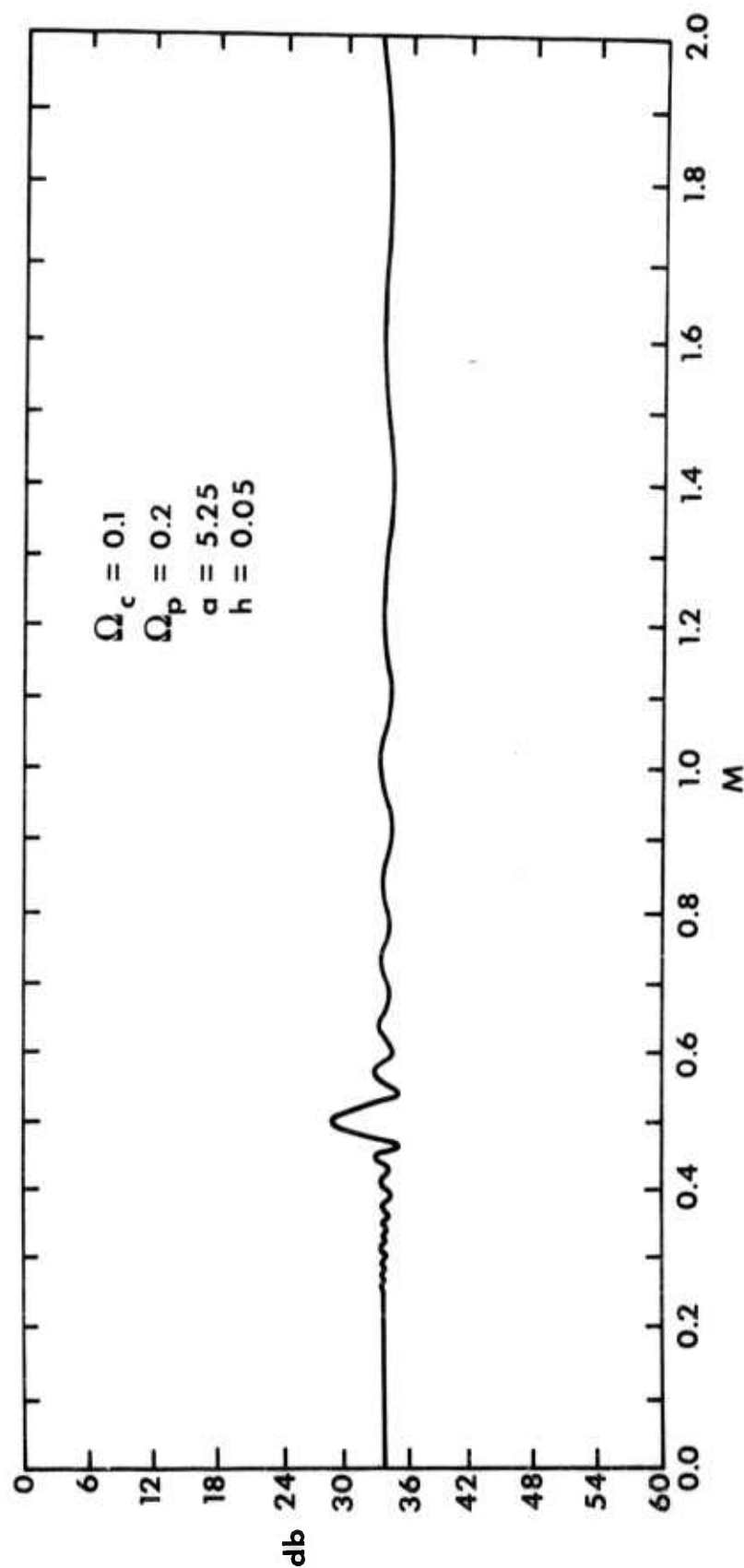


Figure 5 Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.05$

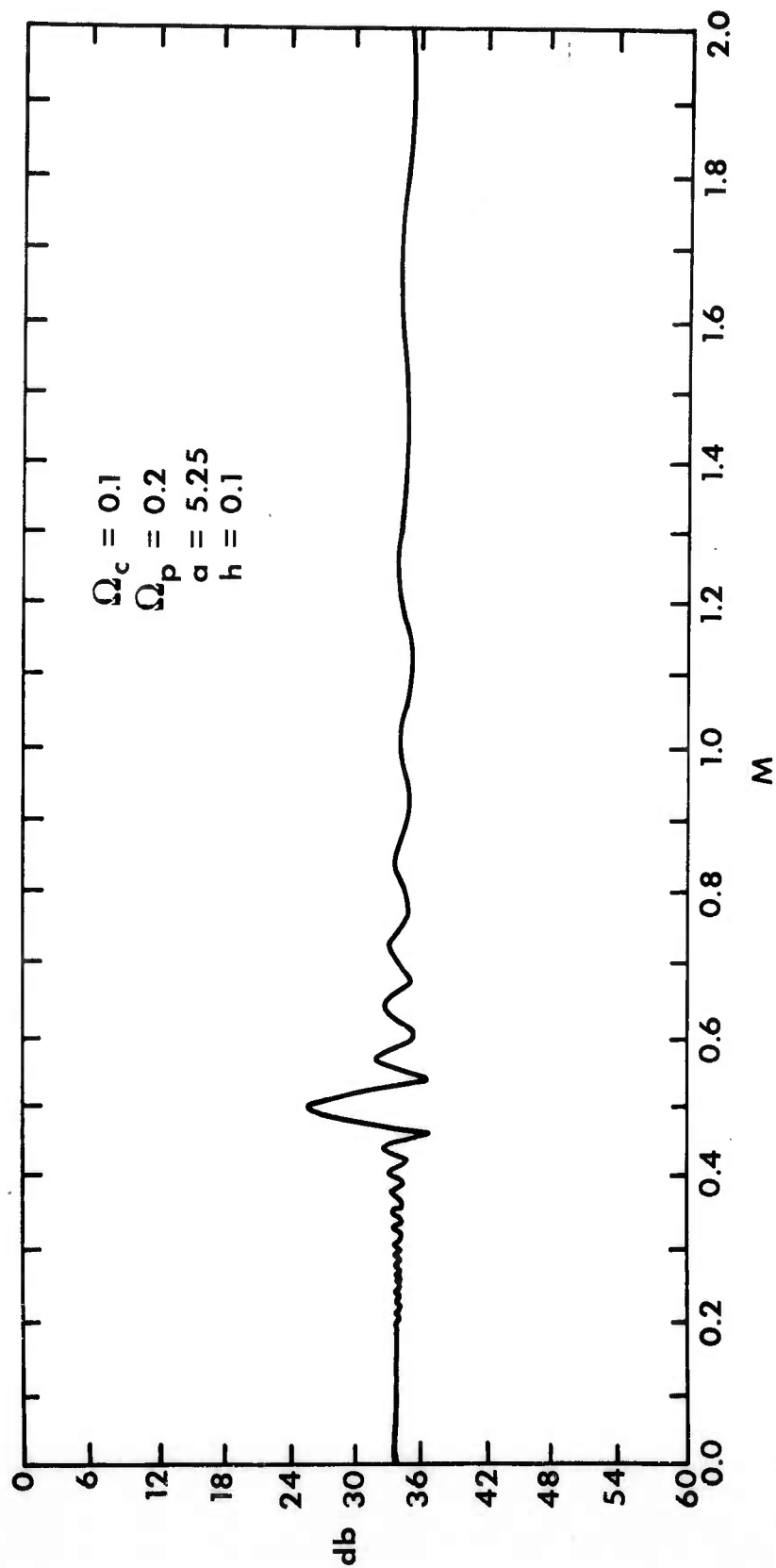


Figure 6 Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.1$

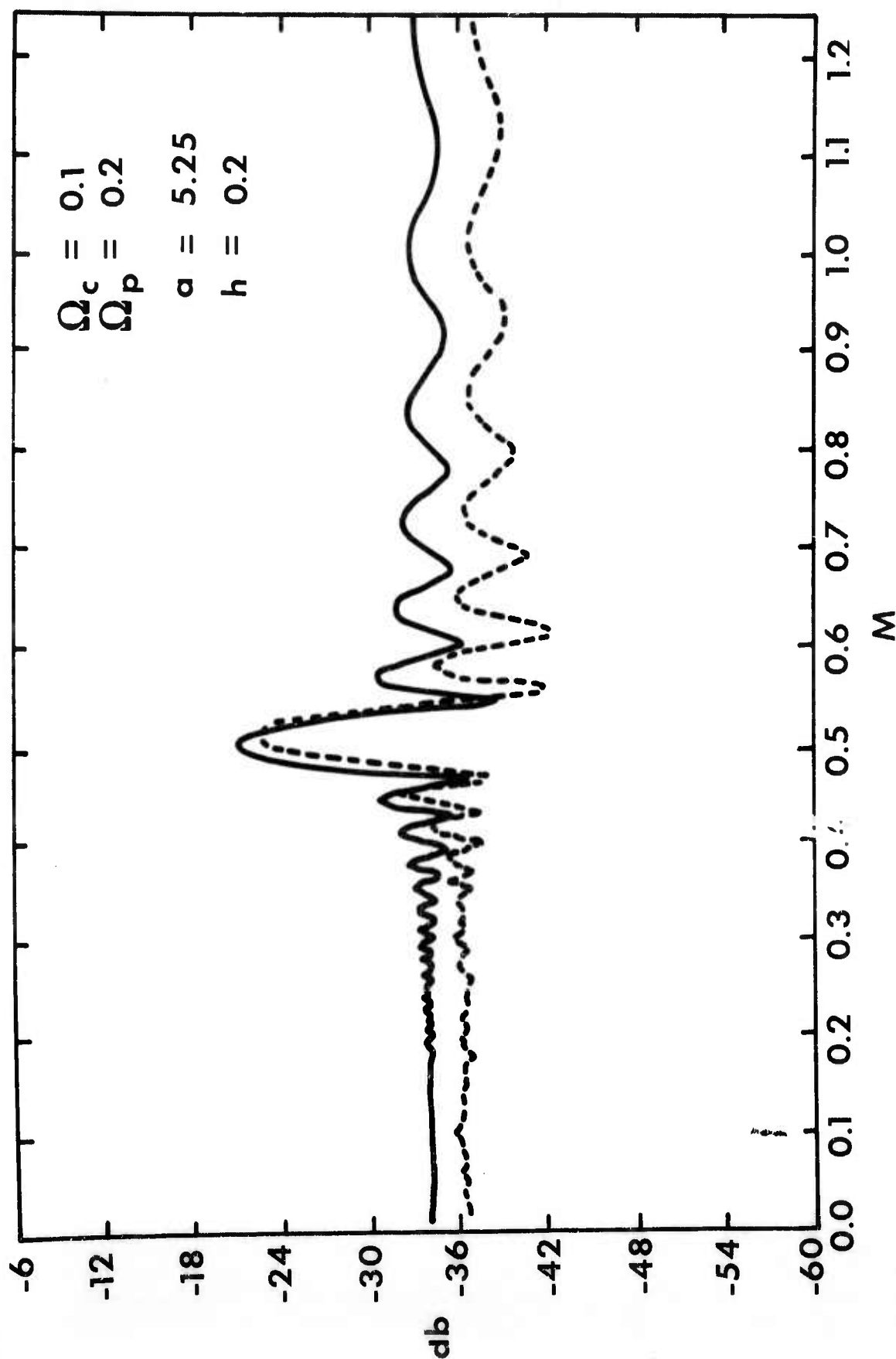


Figure 7 Reflection Coefficient of a Plasma Slab with Harmonic Density Variation as a
 Function of the Normalized Density Wavelength and a Density Modulation $h = 0.2$
 Dashed Line - Exact Values of Reflection Coefficient
 Solid Line - Born Approximation of the Reflection Coefficient

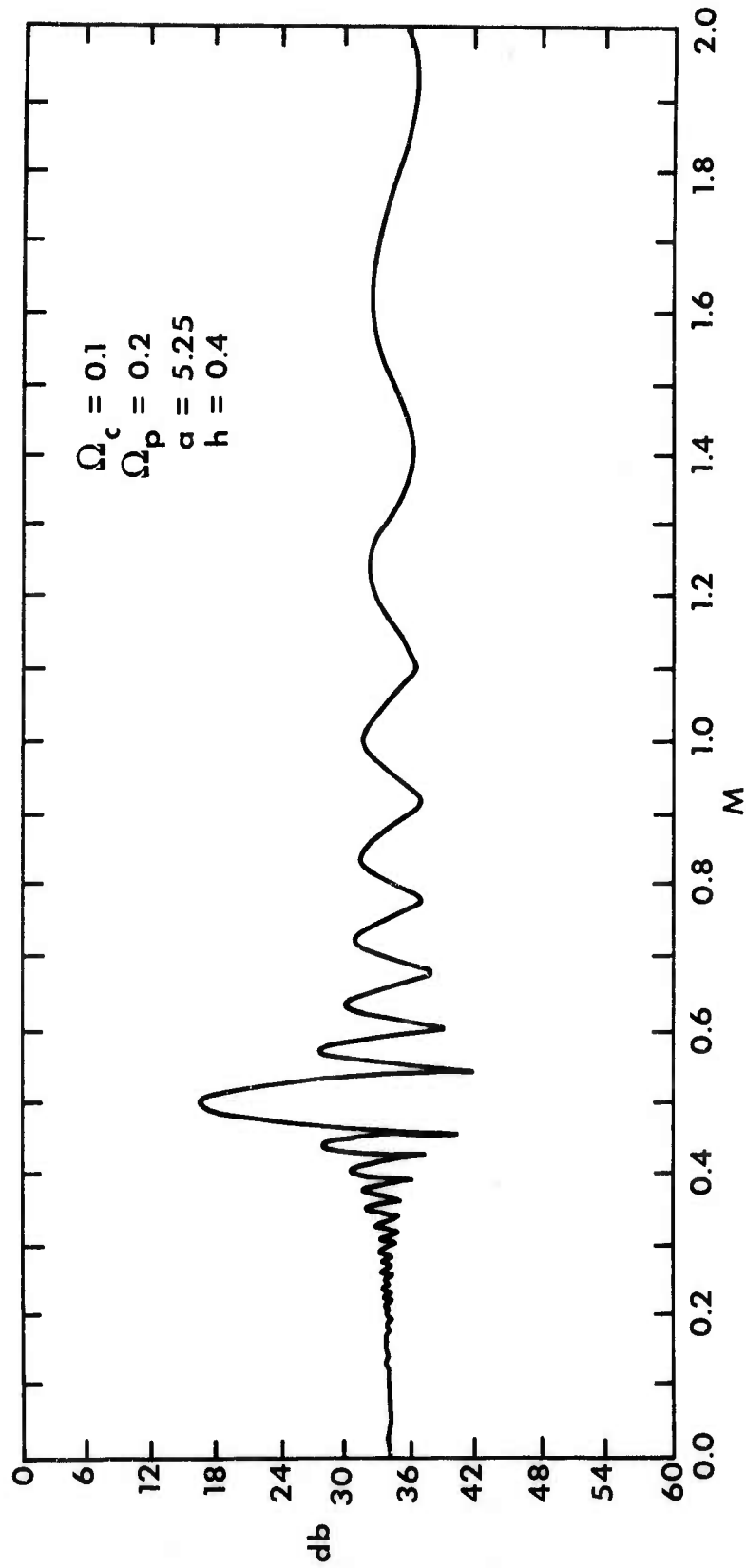


Figure 8 Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.4$

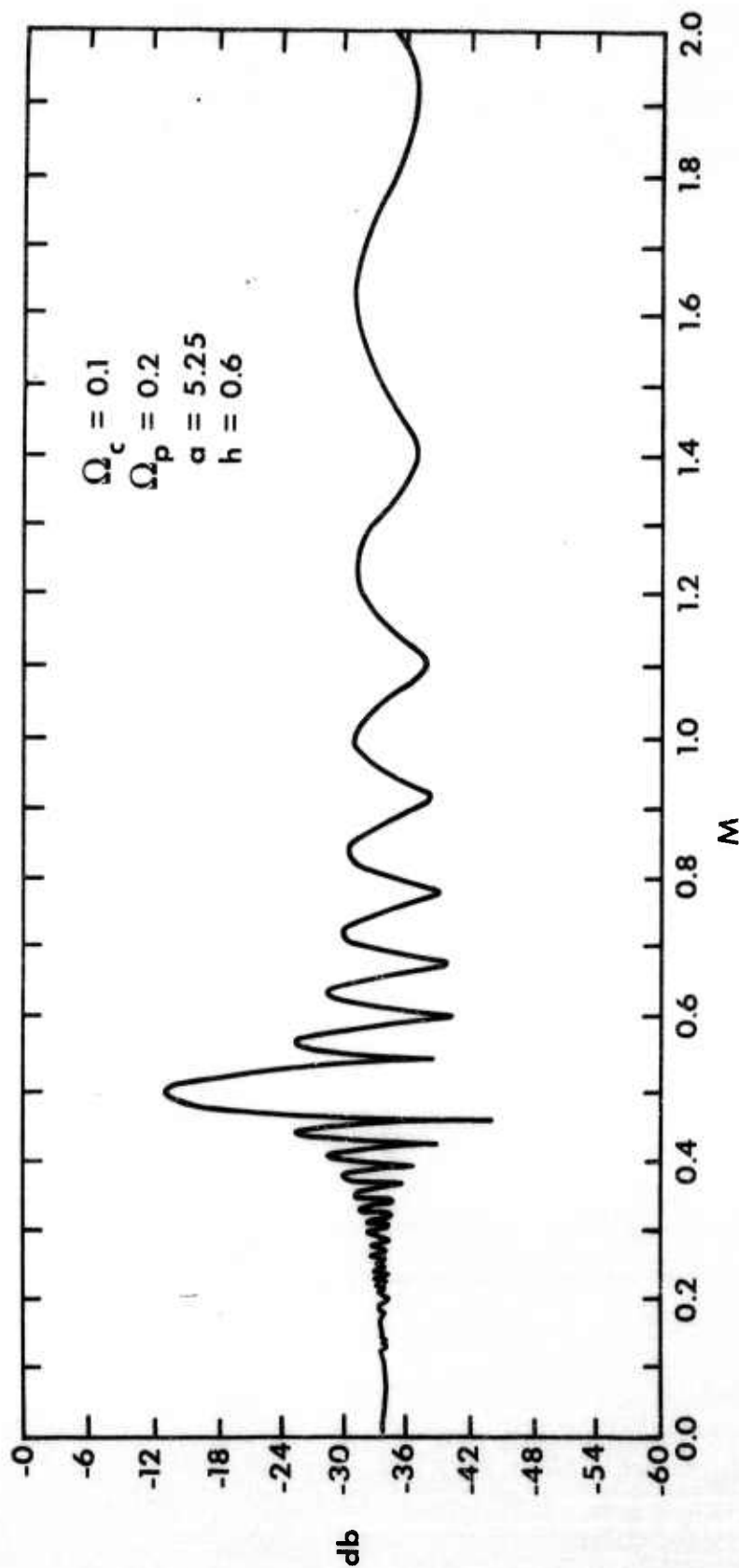


Figure 9 Reflection Coefficient (Born Approximation) of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 0.6$

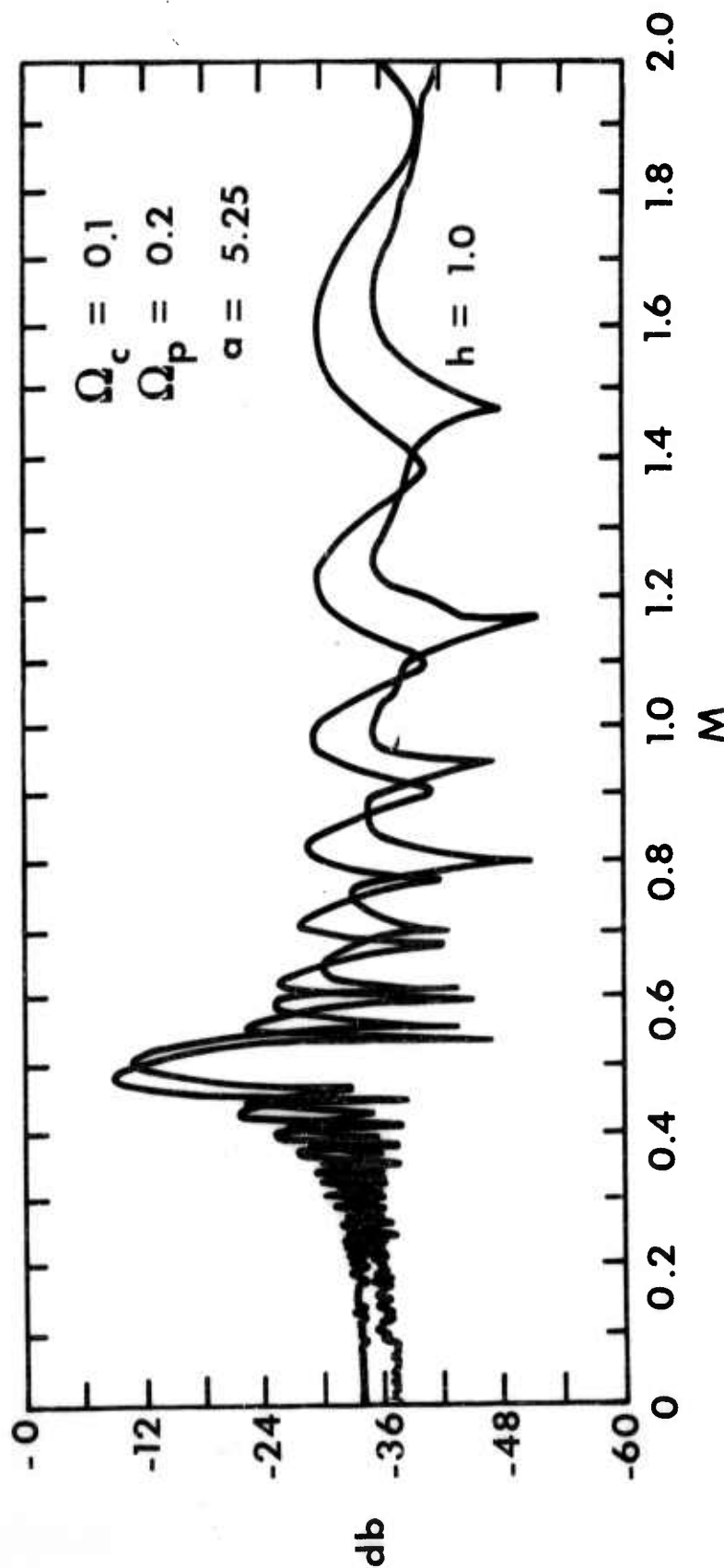


Figure 10 Reflection Coefficient of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 1.0$ and $\alpha = 5.25$

Colored Curve: Exact Values of Reflection Coefficient
 Black Curve: Born Approximation of the Reflection Coefficient

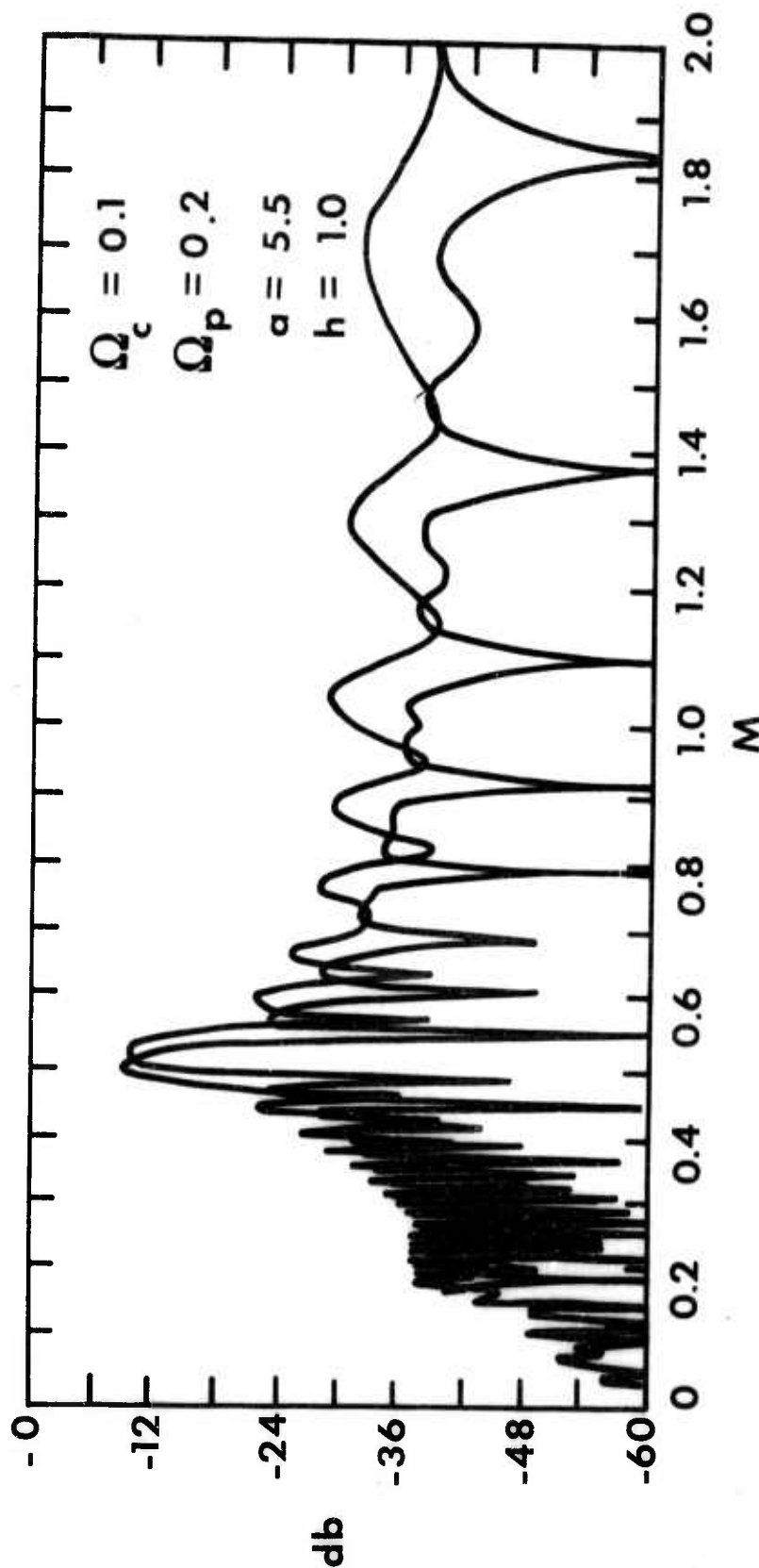


Figure 11 Reflection Coefficient of a Plasma Slab with Harmonic Density Variation as a Function of the Normalized Density Wavelength and a Density Modulation $h = 1.0$ and $a = 5.5$

Colored Curve: Exact Values of Reflection Coefficient
 Black Curve: Born Approximation of the Reflection Coefficient

DISTRIBUTION LIST for Analysis Reports on the HYPERVELOCITY RANGE RESEARCH PROGRAM

<u>Recipient</u>	<u>Copy No.</u>	<u>Recipient</u>	<u>Copy No.</u>
Director		U.S. Air Force	
Advanced Research Projects Agency		Ballistic Systems Division	
Washington 25, D. C.		AF Unit Post Office	
ATTN: F. Koether	1 - 3	Los Angeles 45, California	
ATTN: E. Haynes	4	ATTN: Major W. Levy	51
ATTN: C. McLain	5	ATTN: Lt. K. G. Jefferson	52
ATTN: Major J. Kiernan	6	HQ BSD (AFSC)	
Aerojet-General Corporation		AF Unit Post Office	
P. O. Box 296		Los Angeles 45, California	
Azusa, California		ATTN: BSRVD	53
ATTN: Technical Library	7	USAF Cambridge Research Laboratories	
Aeronutronics Division, Ford Motor Co.		Laurence Hanscom Field	
Ford Road		Bedford, Massachusetts	
Newport Beach, California		ATTN: CRRELRL, Stop 29	54
ATTN: Technical Information Services	8	Director	
ATTN: R. Hoglund	9	USAF Office of Scientific Research	
Aerospace Corporation		Washington 25, D. C.	
2400 E. El Segundo Blvd		ATTN: Mechanics Division	55
El Segundo, California		Major Terrell	
ATTN: Manager of Penetration Aids	10	Director	
Aerospace Corporation		Ames Research Center	
P. O. Box 95085		Moffett Field, California	
Los Angeles 45, California		ATTN: H. Allen	56
ATTN: J. Logan	11	Applied Physics Laboratory	
Aerospace Corporation		The John Hopkins University	
San Bernardino, California		8621 Georgia Avenue	
ATTN: Mr. R. Fowler	12	Silver Spring, Maryland	
ATTN: Mr. Howard Meyers	13-42	ATTN: G. Seielstad	57
Avco-Everett Research Laboratory		Applied Physics Laboratory	
2385 Revere Beach Parkway		Sylvania Elec. Products	
Everett 49, Massachusetts		Waltham, Massachusetts	
ATTN: Dr. Bennett Kivel	43	ATTN: R. Row	58
ATTN: Technical Library	44	Armour Research Foundation	
Avco Research and Advanced Development		10 W. 35th Street	
Wilmington, Massachusetts		Chicago 16, Illinois	
ATTN: Dr. A. Pallone	45	ATTN: Fluid Dynamics Research	59
ATTN: Dr. W. E. Gibson	46	Division	
ATTN: Dr. J. Ekerman	47	Commanding General	
Bell Telephone Laboratories		U. S. Army Air Defense Command	
Murray Hill, New Jersey		Colorado Springs, Colorado	
ATTN: Dr. I. Pelech	48	ATTN: Advanced Projects Division, G-3	60
ATTN: Dr. S. P. Morgan	49		
ATTN: Dr. S. J. Buchsbaum	50		

DISTRIBUTION LIST (continued)

<u>Recipient</u>	<u>Copy No.</u>	<u>Recipient</u>	<u>Copy No.</u>
Commanding General U. S. Army Ballistics Research Laboratories Aberdeen Proving Gound, Maryland ATTN: C. H. Murphy	61	Avco Corporation Research and Advanced Development Division Wilmington, Massachusetts ATTN: Technical Library	76
ATTN: B. J. Karpov	62	ATTN: Dr. Wentink	77
Commanding General U. S. Army Elec. and Communications Command Research and Development Fort Monmouth, New Jersey	63	Special Projects Office Department of The Navy Washington 25, D. C. ATTN: Martin Bloom/SP-272	78
Commanding General U. S. Army Materiel Command Washington 25, D. C.	64	Barnes Engineering Company 30 Commerce Road Stamford, Connecticut ATTN: H. Yates	79
Commander U. S. Army Missile Command Redstone Arsenal, Alabama ATTN: AMSMI-RB	65	Battelle Memorial Institute 505 King Avenue Columbus 1, Ohio ATTN: Battelle-DEFENDER	80
ATTN: AMSMI-RRX	66	Bell Telephone Laboratories, Inc. Whippany, New Jersey	
ATTN: AMSMI-RNR	67	ATTN: C. W. Hoover, Room 2B-105	81
ATTN: AMCPM-ZER-R	68	ATTN: C. E. Paul	82
Security Office, Army Missile Command Pacific Field Office Box 56, Navy 824 c/o FPO, San Francisco, California ATTN: Dr. S. Edelberg	69	ATTN: John McCarthy	83
Commanding General U. S. Army Research and Development Washington 25, D. C. ATTN: Intl. Division	70	Bendix Corporation Systems Division 3300 Plymouth Road Ann Arbor, Michigan ATTN: Systems Analysis and Math Dept.	84
ATTN: Physical Sciences Division	71	ATTN: Flight Sciences Department	85
Commanding Officer U. S. Army Signal Missile Support Agency White Sands Missile Range, New Mexico ATTN: SIGWS-MM-1	72	Boeing Airplane Company P. O. Box 3707 Seattle, Washington ATTN: Org. 2-5732/J. Klaimon	86
ATTN: MEW	73	Brown Engineering Company Huntsville, Alabama ATTN: Technical Library	87
U. S. Army Technical Intelligence Agency Arlington Hall Station Arlington 12, Virginia ATTN: ORDLI	74	California Institute of Technology Pasadena, California ATTN: Prof. L. Lees	88
ARO, Inc. von Karman Facility Tullahoma, Tennessee ATTN: J. Lukasiewicz	75	Central Intelligence Agency 2930 E Street, N. W. Washington, D. C. ATTN: OCR Standard Distribution	89-91

DISTRIBUTION LIST (continued)

<u>Recipient</u>	<u>Copy No.</u>	<u>Recipient</u>	<u>Copy No.</u>
Communication and Propagation Laboratory Stanford Research Institute Menlo Park, California ATTN: Mr. Ray L. Leadabrand, Head		Geophysics Corporation of America Burlington Road Bedford, Massachusetts	123
Propagation Group	92	Heliodyne Corporation	124
ATTN: Dr. Carson Flammer	93	2365 Westwood Blvd Los Angeles 64, California	
Defense Documentation Center	94-113	Institute for Defense Analyses 1666 Connecticut Avenue N.W. Washington 9, D. C.	
Cameron Station Alexandria, Virginia		ATTN: Dr. J. Menkes	125
Cornell Aeronautical Laboratory 4455 Genesee Street Buffalo 21, New York		ATTN: Dr. L. Biberman	126
ATTN: J. Lotsof	114	ATTN: Dr. R. Fox	127
ATTN: W. Wurster	115	ATTN: Dr. J. Martin	128
ATTN: Applied Physics Dept.	116	ATTN: Mr. D. Katcher, JASON Library	129
Defense Research Corporation 6300 Hollister Avenue, Goleta, California ATTN: W. Short	117	Institute of Science and Technology The University of Michigan P. O. Box 618 Ann Arbor, Michigan ATTN: BAMIRAC Library	130
Director Electromagnetic Warfare Laboratory Wright-Patterson Air Force Base Dayton, Ohio ATTN: ASRN/W. Bahret	118	Jet Propulsion Laboratory 4800 Oak Grove Drive Pasadena, California ATTN: H. Denslow	131
Electro-Optical Systems, Inc. 300 N. Halstead Street Pasadena, California ATTN: R. Denison	119	ATTN: Library	132
General Applied Sciences Laboratories Merrick and Stewart Avenues Westbury, Long Island, New York ATTN: M. Bloom	120	Kaman Nuclear Division Colorado Springs, Colorado ATTN: A. Bridges	133
General Dynamics Corporation Astronautics Division San Diego, California ATTN: Chief Librarian, Mail Zone 6-157	121	Director Langley Research Center Langley Field, Virginia ATTN: W. Erickson	134
General Electric Company Re-entry Vehicles Division 3198 Chestnut Street Philadelphia, Pennsylvania ATTN: L. I. Chaseen, Room 3446	122	ATTN: R. L. Trimpi	135
		Lockheed Corporation Missiles and Space Division Sunnyvale, California ATTN: Ray Munson	136
		Melpar, Inc. Applied Science Division 11 Galen Street Watertown 72, Massachusetts ATTN: Librarian	137

DISTRIBUTION LIST (continued)

<u>Recipient</u>	<u>Copy No.</u>	<u>Recipient</u>	<u>Copy No.</u>
Martin Aircraft Company Orlando, Florida ATTN: J. Mays	138	Purdue University School Aero and Engineering Sciences LaFayette, Indiana ATTN: I. Kvakovsky	151
Director Marshall Space Flight Center Huntsville, Alabama ATTN: M-AERO-TS	139	Radio Corporation of America Missiles and Surface Radar Division Moorestown, New Jersey	152
Massachusetts Institute of Technology Lincoln Laboratory P. O. Box 73 Lexington 73, Massachusetts ATTN: M. Herlin	140	The Rand Corporation 1700 Main Street Santa Monica, California ATTN: Library	153
ATTN: R. Slattery	141	Raytheon Manufacturing Company Missile Systems Division Bedford, Massachusetts ATTN: I. Britton, Librarian	154
ATTN: V. Guethlen	142		
Chief U. S. Navy Bureau of Weapons Washington 25, D. C. ATTN: RMWC-322	143	Rome Air Development Center Griffiss Air Force Base Rome, New York ATTN: P. Sandler	155
Chief of Naval Operations Washington 25, D. C. ATTN: OP-07T10	144	The Martin Company Aerospace Division, Mail No. T-38 P. O. Box 179, Denver, Colorado 80201 ATTN: R. E. Compton, Jr.	156
Commander U. S. Naval Ordnance Laboratory White Oak, Silver Spring, Maryland ATTN: Technical Library	145	Space Technology Laboratories, Inc. 1 Space Park Redondo Beach, California ATTN: Leslie Hromas	157
Director U. S. Naval Research Laboratory Washington 25, D. C. ATTN: Code 2027	146	The Warner and Swasey Company Control Instrument Division 32-16 Downing Street Flushing 54, New York	158
New York University Department of Aero Engineering University Heights New York 53, New York ATTN: L. Arnold	147	University of California San Diego, California ATTN: Prof. N. M. Kroll	159
North American Aviation Space and Information Systems Division 12214 Lakewood Blvd Downey, California ATTN: E. Allen	148	University of California Lawrence Radiation Laboratory Livermore, California ATTN: C. Craig	160
Princeton University Princeton, New Jersey ATTN: Prof. E. Frieman	149	Scientific and Technical Information Facility P. O. Box 5700 Bethesda, Maryland ATTN: NASA Representative	161, 162
ATTN: Prof. S. Bogdonoff	150	(SAK/DL-639)	

DISTRIBUTION LIST (Concluded)

<u>Recipient</u>	<u>Copy No.</u>	<u>Recipient</u>	<u>Copy No.</u>
General Electric Company Re-entry Systems Department Missile and Space Division P. O. Box 8555 Philadelphia, Pennsylvania ATTN: Mr. H. W. Ridyard	163	* Commanding Officer U. S. Army Missile Command Redstone Arsenal, Alabama ATTN: SMIDW-B1 (C)	168
University of Michigan Radiation Laboratory 201 Catherine Ann Arbor, Michigan ATTN: R. J. Leite	164	** British Joint Mission British Embassy 3100 Massachusetts Avenue, N. W. Washington, D. C. ATTN: Mr. F. I. Reynolds, Defense Research Staff	169
Valley Forge Space Technical Center General Electric Company P. O. Box 8555 Philadelphia 1, Pennsylvania ATTN: J. Farber	165	** Australian Embassy 2001 Connecticut Avenue N. W. Washington, D. C. ATTN: D. Barnsley, Defense Research and Development Rep.	170
Director Weapons Systems Evaluation Group Pentagon, Room 1E-800 Washington 25, D. C.	166	* University of Toronto Department of Electrical Engineering Toronto, Ontario, Canada ATTN: Mr. H. Treial, Research Associate	171
U. S. Army Liaison Office Canadian Armament Research and Development Establishment P. O. Box 1427 Quebec, P. Q., Canada ATTN: Lt. Col. E. W. Kreischer	167	Capt. L. L. Schoen, USAF USAF Technical Representative c/o GM Defense Research Laboratories	172
		GM Defense Research Laboratories	173 and above

* Unclassified reports only.

** Research reports on hypervelocity ranges and air and contaminant chemistry only – not included for analytical reports on U. S. missile data or classified reports.

Additional Distribution for Semiannual Reports only:

Office of Naval Research Department of the Navy Washington 25, D. C.	
ATTN: Dr. S. Silverman, Science Director	1 copy
ATTN: Dr. F. Isakson, Physics Branch	1 copy
ATTN: Mr. M. Cooper, Fluid Dynamics Branch	1 copy

UNCLASSIFIED

UNCLASSIFIED